

P2.

$$T_A = 290; F = 10; T_{eq} = F T_A$$

$$2900$$

$$PRF = 1500;$$

$$\theta_B = 2;$$

$$\omega_{rpm} = 9;$$

$$n = \frac{\theta_B \times PRF}{6 \times \omega_{rpm}}$$

$$\frac{500}{9}$$

Número de impulsos/ [number of pulses](#) = 55;

$$\tau = 1.5 \times 10^{-6}; B = 1 / (2 \tau);$$

$$\Delta f = B$$

$$3.333 \times 10^5$$

$$P_T = 10^5; \lambda = .3 / 2.7; G = 1000; \sigma_{av} = 10;$$

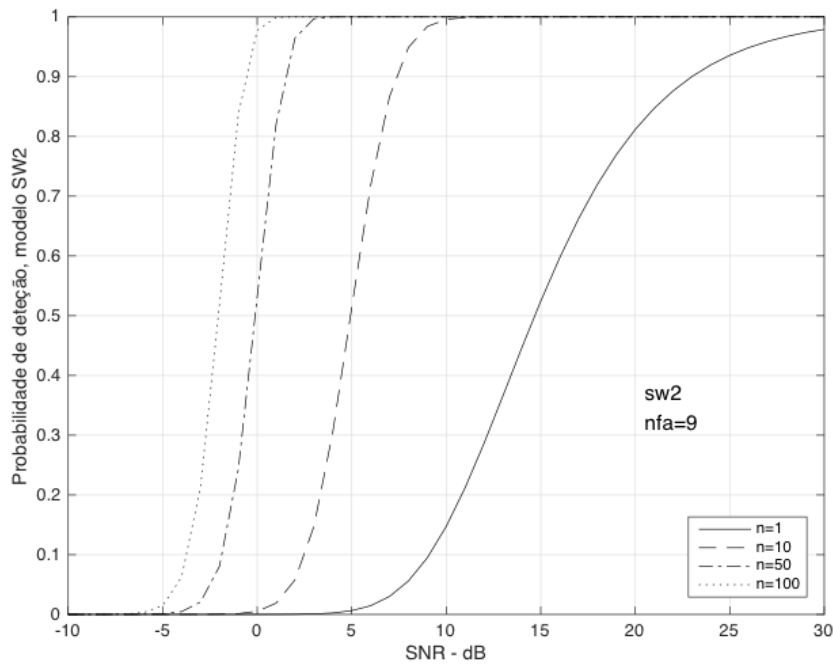
$$K = 1.38 \times 10^{-23};$$

$$R_{max} = \left(\frac{P_T \lambda^2 G^2 \sigma_{av}}{(4 \pi)^3 K T_{eq} \Delta f SN1, 50} \right)^{1/4}$$

(* Nas condições do enunciado vale SW2

SN1dB ≈ 2 ; [according to the stated](#)

[in the problem we consider SW2 and SN1dB \$\approx 2\$ *](#))



$$SN1dB = 2; SN1 = 10^{SN1dB/10}.$$

1.585

$$Rmax = \left(\frac{PT \lambda^2 G^2 \sigma_{av}}{(4 \pi)^3 K T_{eq} \Delta f SN1} \right)^{1/4}$$

131 000.

P 3

$$v = 250; \lambda = 0.03;$$

$$\theta_e = 20^\circ; \theta_a = 30^\circ;$$

$$fd = \frac{2v}{\lambda} \cos[\theta_e] \cos[\theta_a]$$

$$1.356 \times 10^4$$

Como $f_m \approx 2 f_d$, as componentes espectrais em f_d e $f_m - f_d$ podem ser confundidas

As $f_m \approx 2 f_d$, the spectral lines at f_d and $f_m - f_d$ can be mis-interpreted

b)

$$D = \frac{\Delta f}{f_m} \sin(2 \pi f_m R / c)$$

$$J_0(D) = 0 \text{ ocorre para/ (occurs for) } D=2.4$$

$$c = 3 \times 10^8; f_{mod} = 40\,000; \Delta f = 0.5 \times 10^6;$$

$$R = \frac{c}{2 \pi f_{mod}} \text{ArcSin} \left[\frac{2.4 f_{mod}}{\Delta f} \right]$$

230.6

P 4

b)

Velocidade do radar relativa ao solo/ [radar velocity relative to ground](#)

$$v_{\text{radar}} = 600 / 3.6 \rightarrow 166.7 \text{ ms}^{-1}$$

Velocidade relativa entre alvo e rada / [relative velocity radar - target](#)

$$r \rightarrow v_{\text{radar}} + |v_a| = 200 \text{ ms}^{-1}$$

$$f_{\text{GHz}} = 5.25; \lambda = 0.3 / f_{\text{GHz}} \rightarrow \lambda = 0.05714$$

Desvio Doppler do alvo/ [Doppler shift](#),

$$f_d = 2 (v_{\text{radar}} + |v_a|) / \lambda \rightarrow 7000 \text{ Hz}$$

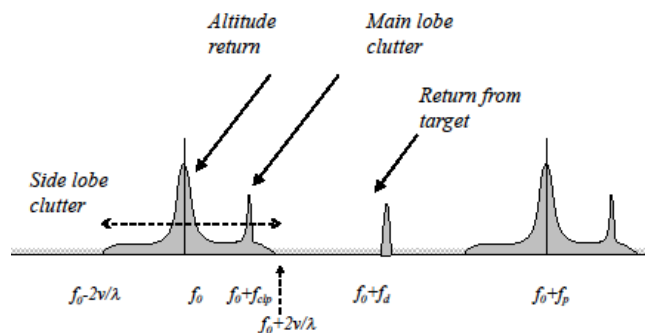
Nota: deverá ser/ [Note: it should be](#)

$$f_d > 2 v_{\text{radar}} / \lambda = 5833 \text{ Hz}$$

$$\text{e /and } f_0 + f_p - (f_0 + f_d) > 2 v_{\text{radar}} / \lambda$$

isto é/ [that is](#)

$$f_p > 2 v_{\text{radar}} / \lambda + f_d \rightarrow f_p > 12.83 \text{ pps (kHz)}$$

ou seja/ [thus](#) \rightarrow $f_{p\text{min}} = 12.83 \text{ kHz}$ 

c)

posição do desvio Doppler do alvo a1

[Doppler shift for target a1](#)

$$v_{a1} = -250 / 3.6 \rightarrow -69.44 \text{ ms}^{-1}$$

$$f_{da1} = 2 (v_{\text{radar}} - |v_{a1}|) / \lambda \rightarrow 3403 \text{ Hz}$$

posição do desvio doppler do alvo 2

[Doppler shift for target 2](#)

$$v_{a2} = 250 / 3.6 \rightarrow 69.44 \text{ ms}^{-1}$$

$$f_{da2} = 2 (v_{\text{radar}} + |v_{a2}|) / \lambda \rightarrow 8264 \text{ Hz}$$

extensão do espectro do clutter de solo

[extension of the clutter Doppler spectrum due to ground](#)

$$2 v_{\text{radar}} / \lambda \rightarrow 5833 \text{ Hz}$$

A posição do desvio doppler do alvo 1 encontra-se incluída no espectro do clutter, logo o cancelamento poderá não ser efetivo. O oposto sucede para o alvo 2.

Doppler shift for target 1 is within the clutter spectrum, thus cancellation is not guaranteed.
The opposite prevails for target 2